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Name \_\_\_\_\_ Index No. \_\_\_\_\_

2707/302  
**STRUCTURES III**  
 Oct./Nov. 2015  
 Time: 3 hours

Candidate's Signature \_\_\_\_\_

Date \_\_\_\_\_



**THE KENYA NATIONAL EXAMINATIONS COUNCIL**  
**DIPLOMA IN CIVIL ENGINEERING**  
**MODULE III**  
**STRUCTURES III**  
**3 hours**

**INSTRUCTIONS TO CANDIDATES**

*Write your name and index number in the spaces provided above.*

*Sign and write the date of the examination in the spaces provided above.*

*You should have scientific calculator for this examination.*

*This paper consists of EIGHT questions.*

*Answer any FIVE of the following EIGHT questions in the spaces provided in this question paper.*

*All questions carry equal marks.*

*Maximum marks for each part of a question are as shown.*

*Answers should be written in the spaces provided in this question paper.*

*Candidates should answer the questions in English.*

**For Examiner's Use Only**

Question	1	2	3	4	5	6	7	8	TOTAL SCORE
Candidate's Score									

**This paper consists of 16 printed pages.**

**Candidates should check the question paper to ascertain that all the pages are printed as indicated and that no questions are missing.**

1. A 150 mm thick reinforced concrete slab is supported on simply supported beams of effective length 6 m, spaced at 3 m centres. Select a suitable UB section for the internal beams in grade S275 (grade 43) steel and check for shear, bending and deflection given the following information:

- Characteristic loads:
  - imposed load =  $3.0 \text{ kN/m}^2$
  - Finishes =  $0.8 \text{ kN/m}^2$
  - Unit weight of concrete =  $24 \text{ kN/m}^3$
- $E = 210 \text{ kN/mm}^2$

Ignore the self weight of the beam.

(20 marks)

2. (a) With the aid of labelled sectional sketches, describe the following types of riveted joints:

- (i) lap joint
- (ii) double cover butt joint.

(6 marks)

- (b) A single unequal angle section,  $100 \times 75 \times 10 \text{ mm}$  is welded to a gusset plate as shown in figure 1. It transmits a load  $P$  of  $150 \text{ kN}$  through its centroid. Design the joint using  $8 \text{ mm}$  fillet welds.

Permissible stress in weld =  $100 \text{ N/mm}^2$ .

(14 marks)

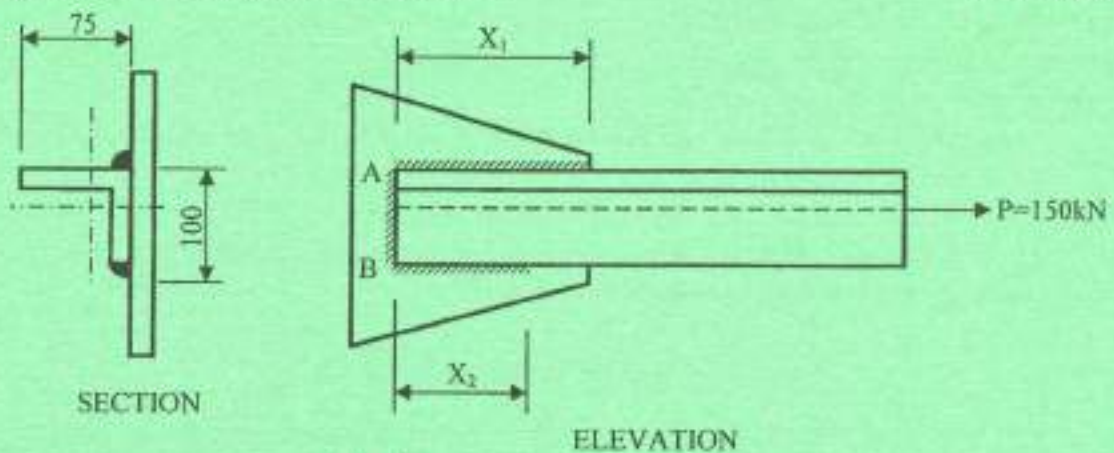


Fig. 1

3. A timber section  $150 \times 150 \text{ mm}$  of strength class C 16 and effective span  $3.0 \text{ m}$  is used as a simply supported beam. Assuming the beam is fully laterally restrained, check the adequacy of the timber beam in bearing, shear, bending and deflection given the following information:

- dead load =  $0.5 \text{ kN/m}$
- imposed load =  $1.5 \text{ kN/m}$
- bearing length =  $100 \text{ mm}$
- take all  $k$  factors to be  $1.0$

(20 marks)

4. Using the three moments theorem, analyze the beam shown in figure 2 and hence sketch the bending moment and shear force diagrams indicating the values at the critical points. (20 marks)

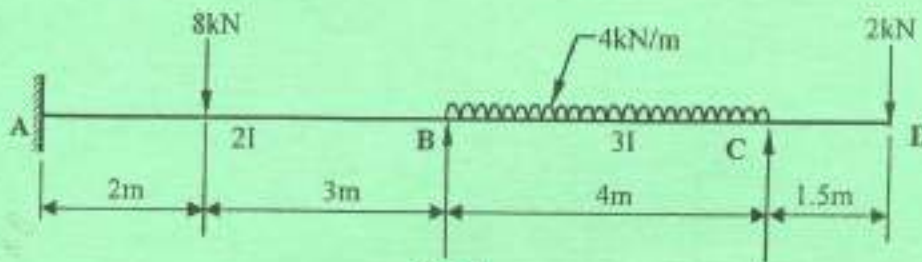


Fig. 2

5. Using the moment distribution method, analyze the beam shown in figure 3 and hence sketch the bending moment diagram indicating the values at the critical points. (20 marks)

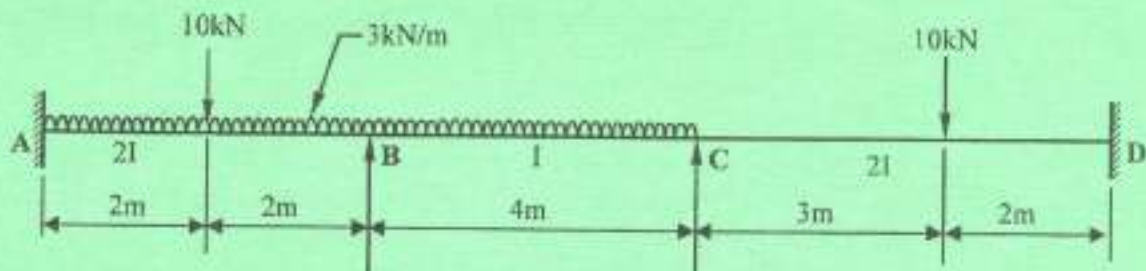


Fig. 3

6. (a) Using Rankines formula, calculate the crippling load that a solid steel rod 4 m long and 50 mm diameter can carry when used as a column with both ends pinned.

Take -  $E = 200 \text{ kN/mm}^2$   
 - Rankines constant,  $a = 1/7500$   
 - crushing stress,  $\sigma_{cs} = 320 \text{ N/mm}^2$  (6 marks)

- (b) An equal angle section 100 x 100 x 8 mm is used as a strut of 3 m length with both ends fixed.

Calculate the crippling load using Euler's formula.  
 Take  $E = 200 \text{ kN/mm}^2$  (14 marks)



7. Figure 4 shows the section of a short rectangular column with a square hole. The column carries an eccentric load  $P$  of 150 kN. Calculate the stresses at the four extreme corners of the column. (20 marks)

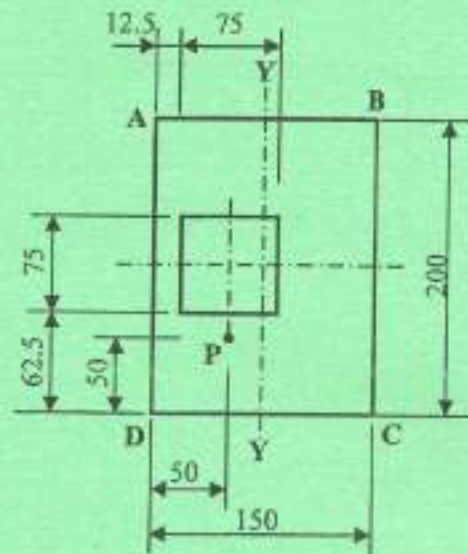


Fig. 4

8. (a) Figure 5 shows a simply supported girder of 8 m span. Using equilibrium conditions, sketch the influence line diagrams for the following load components, calculating values at every 2 m intervals:
- reaction at A
  - shear force at C
  - bending moment at C

(14 marks)

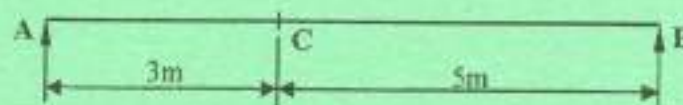
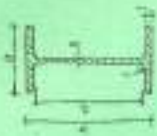


Fig. 5

- (b) If a point load of 60 kN moves across the girder shown in figure 5 from the left to the right, determine the following values using the influence line diagrams.
- maximum reaction at A.
  - maximum positive and negative shear forces at C.
  - maximum bending moment at C.

(6 marks)



Universal beams – dimensions and properties

UB designation	Mass per metre	Depth of section	Web thickness		Depth between flanges	Radius for local buckling		Section moment of area		Radius of gyration		Elastic modulus		Plastic modulus		Buckling parameter	Torsional inertia	Warping constant	Torsional constant	Area of webflange
			Web	Flange		Web	Flange	$I_{xx}$	$I_{yy}$	$r_{xx}$	$r_{yy}$	$Z_{xx}$	$Z_{yy}$	$S_{xx}$	$S_{yy}$					
457 x 152 x 40	39.8	457	8.1	13.3	10.2	407.8	3.29	30.3	25940	195	18.3	1122	104	3287	742	0.868	37.5	0.387	33.8	76.2
457 x 152 x 52	52.1	457	8.1	13.3	10.2	407.8	6.99	53.6	21310	545	17.5	200	84.6	1096	132	0.850	43.9	0.311	31.4	67.6
457 x 178 x 40	37.2	457	9.5	16	10.2	360.4	3.81	37.9	27310	194	17	1225	122	1501	207	0.882	37.5	0.508	33.8	64.5
457 x 178 x 52	49.7	457	9.5	16	10.2	360.4	8.25	41	24300	1385	16.8	1188	153	1548	217	0.95	43.9	0.433	31.4	61.5
457 x 178 x 60	60.1	457	10.8	17.8	10.2	360.4	8.95	45.6	21800	200	16.8	1063	130	1199	206	0.98	33.8	0.456	31.4	58.5
457 x 178 x 76	81.1	457	12.7	20.9	10.2	360.4	8.13	48.8	18730	1021	16.5	930	115	1055	118	0.971	38.3	0.392	33.1	61
457 x 191 x 46	45	457	8.1	13.3	10.2	360.4	8.20	33	15840	536	18.4	778	75.7	828	118	0.871	38.3	0.207	19	58.6
457 x 191 x 58	58	457	8.1	13.3	10.2	360.4	8.24	56.3	12910	410	15.9	658	57.8	724	90.3	0.858	47.5	0.153	10.7	40.7
457 x 191 x 67	67.1	457	8.1	13.3	10.2	360.4	5.33	24.2	16480	1382	15.1	1071	157	1211	263	0.905	34.4	0.412	33.8	65.5
457 x 191 x 77	81.1	457	8.1	13.3	10.2	360.4	5.82	38.5	16030	1108	14.9	934	139	1070	198	0.862	38.3	0.33	32.4	65.6
457 x 191 x 85	91.1	457	8.1	13.3	10.2	360.4	7.46	42.1	14740	948	14.8	786	113	866	174	0.981	32.1	0.386	33.8	64.9
457 x 191 x 95	101.1	457	8.1	13.3	10.2	360.4	8.82	44.5	12070	811	14.5	537	94.8	775	167	0.974	36.8	0.237	15.8	57.3
457 x 214 x 39	36.1	457	6.6	10.7	10.2	311.8	3.89	47.2	10370	388	14.3	576	56.8	638	99.1	0.871	35.2	0.155	15.1	48.8
457 x 214 x 52	49.1	457	6.6	10.7	10.2	311.8	7.38	51.5	8249	280	14	473	44.7	543	70.3	0.863	42.2	0.081	8.78	42.1
457 x 214 x 64	64.1	457	6.6	10.7	10.2	311.8	6.99	37.6	11700	1601	13	750	127	840	189	0.889	33.8	0.234	14.8	68.8
457 x 214 x 77	81.1	457	6.6	10.7	10.2	311.8	7.42	30.6	8859	856	13	640	108	720	146	0.807	37.1	0.195	12.2	58.7
457 x 214 x 85	91.1	457	6.6	10.7	10.2	311.8	8.49	45.2	8033	764	12.9	550	92.6	623	142	0.859	31	0.164	14.7	51.3
457 x 227 x 40	48.3	457	8.1	13.3	10.2	311.8	4.67	25.5	9575	480	12.9	616	73.8	711	116	0.875	33.2	0.102	11.8	61.3
457 x 227 x 46	55.1	457	8.1	13.3	10.2	311.8	5.14	31.1	8195	389	12.4	574	62.6	614	93.4	0.872	26.5	0.085	11.1	53.8
457 x 227 x 52	61.1	457	8.1	13.3	10.2	311.8	5.77	37.4	7171	336	12.2	471	54.5	539	85.4	0.832	28.7	0.072	14.8	47.2
457 x 227 x 64	81.1	457	8.1	13.3	10.2	311.8	4.74	41.8	6501	194	12.5	418	37.9	481	60	0.856	31.4	0.044	12.2	41.8
457 x 227 x 77	101.1	457	8.1	13.3	10.2	311.8	5.78	46	5388	150	12.2	348	30.5	402	43.5	0.859	27.4	0.035	7.4	35.9
457 x 227 x 85	111.1	457	8.1	13.3	10.2	311.8	7.28	47.6	4855	121	11.9	282	24.2	342	38.8	0.866	43.4	0.027	4.77	31.6
457 x 254 x 46	45	457	7.2	12.7	7.6	275.9	5.8	30.8	6548	677	10.9	504	92	566	141	0.801	21.2	0.103	13.9	64.8
457 x 254 x 58	58	457	7.2	12.7	7.6	275.9	6.72	34.8	5537	571	10.6	453	78	483	119	0.809	24.2	0.036	15.3	47.2
457 x 254 x 70	70	457	7.2	12.7	7.6	275.9	8.49	38.5	4413	468	10.1	361	61.3	390	94.1	0.88	20.6	0.028	8.33	35.7
457 x 254 x 85	85	457	7.2	12.7	7.6	275.9	11.1	35.7	4005	179	10.5	306	34.9	355	54.6	0.874	21.5	0.023	8.57	36.1
457 x 254 x 102	102	457	7.2	12.7	7.6	275.9	8.07	37.5	3412	146	10.1	266	28.2	306	46	0.869	31.5	0.023	6.42	32
457 x 254 x 127	127	457	7.2	12.7	7.6	275.9	7.67	35.5	2841	111	10.1	224	23.5	250	37.3	0.816	36.4	0.018	4.15	28
457 x 305 x 39	39	457	6.4	9.6	7.6	275.9	5.97	25.9	2466	381	8.71	289	57.5	314	38.2	0.881	21.5	0.037	10.3	38.2
457 x 305 x 52	52	457	6.4	9.6	7.6	275.9	8.54	30.7	2340	308	8.58	225	46.2	258	70.9	0.877	25.8	0.029	5.96	31
457 x 305 x 70	70	457	6.4	9.6	7.6	275.9	5.47	31.4	2105	194	8.46	207	32.2	234	48.3	0.868	22.5	0.015	7.82	29.8
457 x 305 x 85	85	457	6.4	9.6	7.6	275.9	5.41	30.6	1556	137	7.48	152	27	171	41.8	0.888	22.8	0.01	4.41	24.2
457 x 305 x 118	118	457	6.4	9.6	7.6	275.9	5.78	27.1	654	89.8	6.41	109	20.2	133	31.3	0.89	15.6	0.005	1.96	20.2
457 x 305 x 13	13	457	6.4	9.6	7.6	275.9	3	24.1	479	55.7	6.38	94.8	18.1	65.2	22.8	0.895	16.3	0.003	2.33	16.5

Table 3 — Grade stresses and moduli of elasticity for various strength classes: for service classes 1 and 2

Strength class	Bending parallel to grain $N/mm^2$	Tension parallel to grain $N/mm^2$	Compression parallel to grain $N/mm^2$	Compression perpendicular to grain* $N/mm^2$	Shear parallel to grain $N/mm^2$	Modulus of elasticity		Characteristic density, $\rho_k$ , <sup>b</sup> $kg/m^3$	Average density, $\rho_{ave}$ , <sup>b</sup> $kg/m^3$
						Mean $N/mm^2$	Minimum $N/mm^2$		
C14	4.1	2.5	5.2	2.1	1.6	0.60	6 800	290	350
C16	5.3	3.2	6.8	2.2	1.7	0.67	8 800	310	370
C18	5.8	3.5	7.1	2.2	1.7	0.67	9 100	320	380
C22	6.8	4.1	7.5	2.3	1.7	0.71	9 700	340	410
C24	7.5	4.5	7.9	2.4	1.9	0.71	10 800	350	420
C27	10.0	6.0	8.2	2.5	2.0	1.10	12 300	370	450
C30	11.0	6.5	8.6	2.7	2.2	1.20	12 300	380	460
C35	12.0	7.2	8.7	2.9	2.4	1.30	13 400	400	480
C40	13.0	7.8	8.7	3.0	2.6	1.40	14 500	420	500
D30	9.0	5.4	8.1	2.8	2.2	1.40	9 500	530	640
D35	11.0	6.5	8.5	3.4	2.6	1.70	10 000	560	670
D40	12.5	7.5	12.6	3.9	3.0	2.00	10 800	590	700
D50	16.0	9.5	15.2	4.5	3.5	2.20	15 000	650	780
D60	18.0	10.9	18.0	5.2	4.0	2.40	18 500	700	840
D70	23.0	13.8	23.0	6.0	4.6	2.60	21 000	900	1 080

NOTE: Strength classes C14 to C40 are for softwoods and D30 to D70 are for hardwoods.

\* When the specification specifically prohibits, wane at bearing areas, the higher values of compressions perpendicular to grain stress may be used, otherwise the lower values apply.

† The values of characteristic density given above are for wane when designing joints. For the calculation of dead load, the average density should be used.

