

Name: _____

Index No.: _____

2705/302 2710/302

Candidate's Signature: _____

2709/302

Date: _____

STRUCTURES III

Oct./Nov. 2015

Time: 3 hours

**THE KENYA NATIONAL EXAMINATIONS COUNCIL**

**DIPLOMA IN BUILDING TECHNOLOGY
DIPLOMA IN ARCHITECTURE
MODULE III**

STRUCTURES III

3 hours

**INSTRUCTIONS TO CANDIDATES***Write your name and index number in the spaces provided above.**Sign and write the date of the examination in the spaces provided above.**You should have Mathematical tables/Scientific calculator and drawing instruments for this examination.**This paper consists of EIGHT questions.**Answer any FIVE of the EIGHT questions in the spaces provided in this question paper.**All questions carry equal marks.**Maximum marks for each part of a question are as indicated.**Relevant design tables are attached.**Do NOT remove any pages from this booklet.**Candidates should answer the questions in English.***For Examiner's Use Only**

Question	1	2	3	4	5	6	7	8	TOTAL SCORE
Candidate's Score									

This paper consists of 20 printed pages.

**Candidates should check the question paper to ascertain that
all the pages are printed as indicated and that no questions are missing.**

1. (a) State **three** advantages of the following connections:

(i) Bolted connections;

(ii) Welded connections.

(6 marks)

(b) Figure 1 shows a bolted connection required to transmit a tensile force of 250 kN. Check the adequacy of the joint in terms of:

(i) Tensile stress in plates;

(ii) Tensile stress in angles;

(iii) shear stress in bolts;

(iv) Bearing stress in angles.

(14 marks)

Take the area of an 89 x 76 x 7.8 mm angle to be 12.35 cm².

Permissible tensile stress = 155 N/mm²

Permissible shear stress = 80 N/mm²

Permissible bearing stress = 250 N/mm²

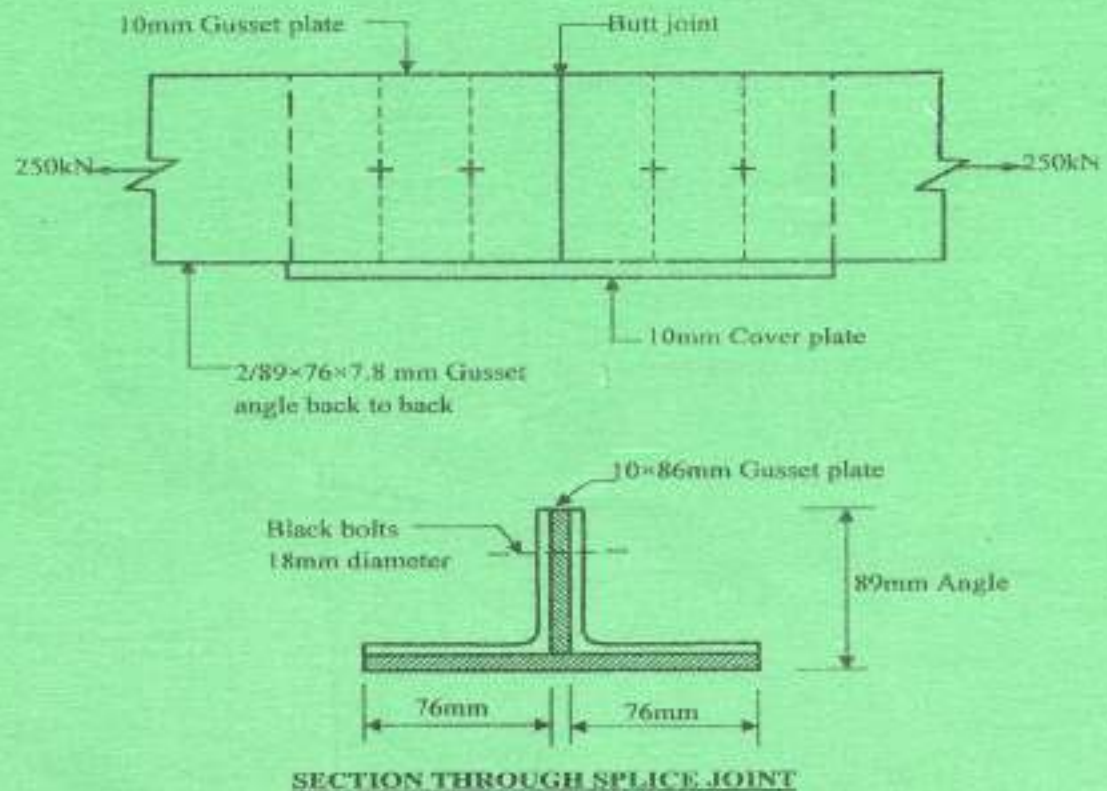


Fig. 1

2. (a) State **four** advantages of casing a steel section. (4 marks)
- (b) A universal column used as an edge stanchion in a multi-storey building has an actual length of 3.6 m centre to centre of floor beam. The loading in the beam is as shown in figure 2. Design the stanchion as an encased column in Grade 43 steel, using the tables provided. (16 marks)

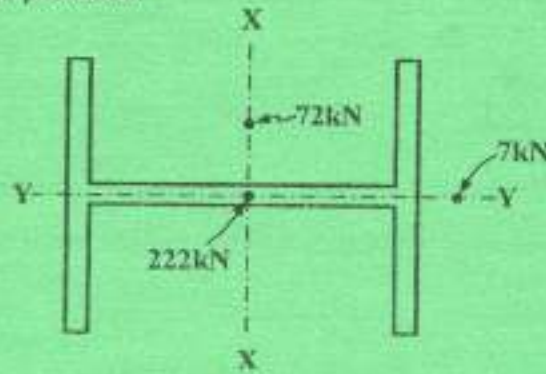


Fig. 2



3. (a) Define the following terms as used to structure timber:
- (i) Basic stress;
 - (ii) Green stress;
 - (iii) Grade stress.
- (3 marks)

- (b) A solid timber column of 200 mm x 150 mm and of strength of class 50 s is 4 m long. It is restrained in position and direction at both ends and is required to carry an axial load of 85 kN. Check the adequacy of the column.

- Table 9 BS 5268
- Grade stress parallel to grain = 8.7 N/mm²
- Eminimum = 7.1 N/mm²
- $K_y = 1.25$, $K_g = 1.0$, for medium duration.

(17 marks)

4. Using the moment distribution method, analyse the beam in figure 3 and sketch the bending moment diagram, indicating all critical values. (20 marks)

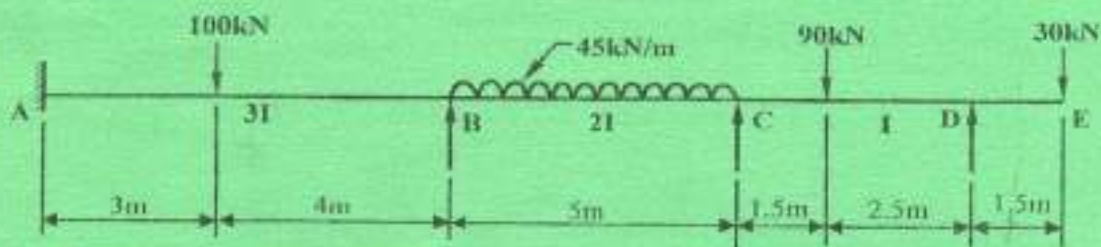


Fig. 3

5. Using the three moment theorem, analyse the beam shown in figure 4 and hence sketch the shear force and bending moment diagrams, indicating values at all critical points. (20 marks)

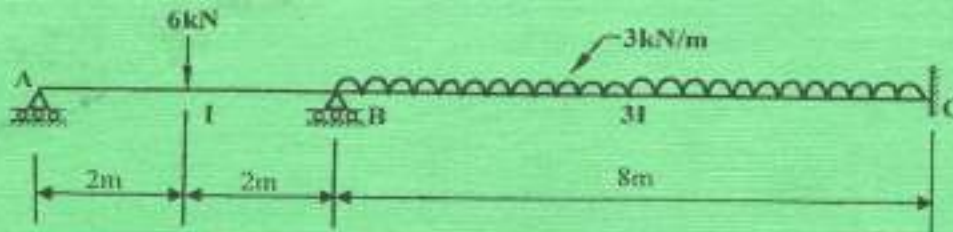


Fig. 4

6. Analyse the frame in figure 5 using moment of distribution method and then plot bending moment diagram, showing the values at all critical points. (20 marks)

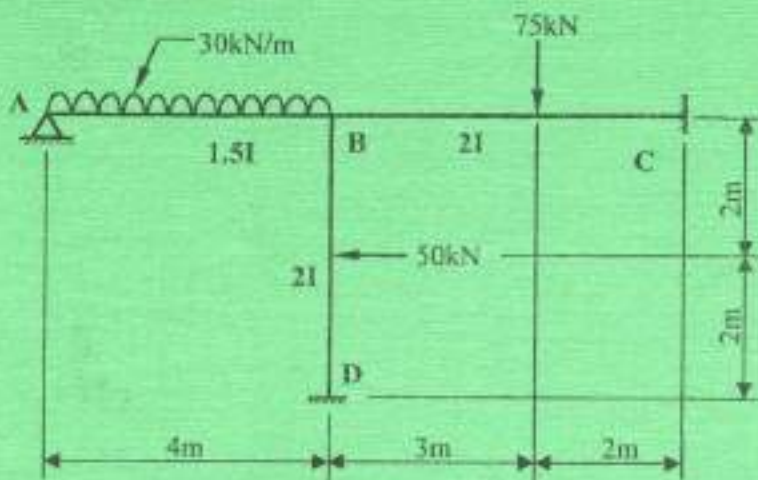


Fig. 5



7. (a) Figure 6 is a simply supported universal beam loaded as shown. Using the data provided below, check if a 533 x 165 x 73 kg/m UB will be satisfactory and hence check for shear and deflection.

Data

- Live loads = 75% of point load
- Compression flanges fully restrained
- $P_y = 100 \text{ N/mm}^2$
- $E = 210 \text{ KN/mm}^2$

(9 marks)

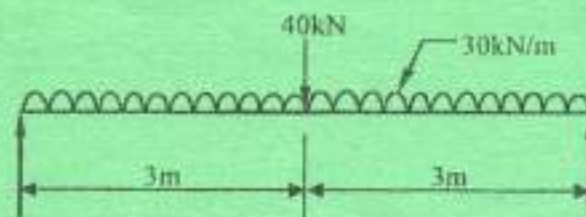


Fig. 6

- (b) (i) Sketch any two butt welds.
- (ii) Design the connection in figure 7 shown using balanced weld design. (11 marks)

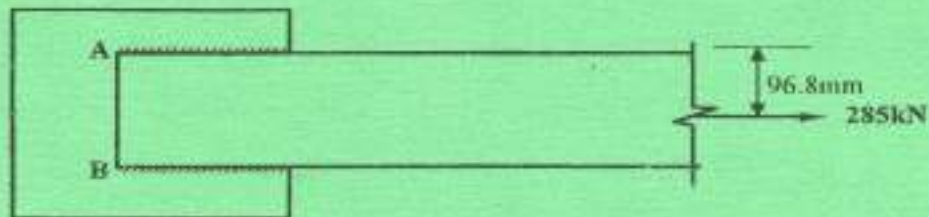


Fig. 7

8. (a) State five properties of structural timber as a construction material. (5 marks)
- (b) A timber having a clear span of 6.0 m is suspended on 250 mm bearing at each end. The beam carries a uniformly distributed load of 15 kN/m over the entire span.

Design the beam using the following information:

- Permissible deflection = span/300
- Permissible shear stress = 1.2 N/mm²
- Depth of section is twice the breadth
- Young's modulus of elasticity, E = 8 kN/mm²

(15 marks)





UNIVERSAL COLUMNS
Parallel Flanges

DIMENSIONS AND PROPERTIES

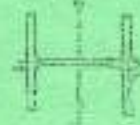
Level Type	No. of panels	Depth of flange D ₁	Width of flange B	Thickness			Depth between flanges D ₂	Area of flanges A _f
				W ₁	W ₂	W ₃		
300 x 400	1E	210	424.4	47.6	77.0	15.2	200.1	809.1
	2E	424.7	424.7	47.6	77.0	15.2	200.1	1618.2
	3E	638.7	419.5	47.6	77.0	15.2	200.1	2427.3
	4E	852.6	412.4	35.8	64.0	15.2	200.1	3236.4
	5E	1066.5	407.0	30.6	49.2	15.2	200.1	4045.5
	6E	1280.4	403.0	27.5	42.9	15.2	200.1	4854.6
	7E	1494.3	399.2	24.5	36.5	15.2	200.1	5663.7
	8E	1708.2	395.2	21.5	30.2	15.2	200.1	6472.8
	9E	1922.1	391.0	18.5	23.8	15.2	200.1	7281.9
	10E	2136.0	387.0	15.5	17.4	15.2	200.1	8091.0
300 x 300	1E	210	424.4	48.0	82.2	15.2	200.1	822.2
	2E	427.0	424.4	48.0	82.2	15.2	200.1	1644.4
	3E	644.0	376.4	76.0	110.0	15.2	200.1	2466.6
	4E	861.0	276.1	64.5	78.0	15.2	200.1	3288.8
	5E	1078.0	202.2	53.0	56.0	15.2	200.1	4111.0
	6E	1295.0	152.3	41.5	34.0	15.2	200.1	2933.2
	7E	1512.0	102.4	30.0	12.0	15.2	200.1	1755.4
	8E	1729.0	52.5	18.5	0.0	15.2	200.1	577.6
	9E	1946.0	2.6	7.0	-1.5	15.2	200.1	-400.2
	10E	2163.0	-27.3	-15.0	-28.0	15.2	200.1	-822.4
300 x 200	1E	210	424.4	48.0	82.2	15.2	200.1	822.2
	2E	427.0	424.4	48.0	82.2	15.2	200.1	1644.4
	3E	644.0	376.4	76.0	110.0	15.2	200.1	2466.6
	4E	861.0	276.1	64.5	78.0	15.2	200.1	3288.8
	5E	1078.0	202.2	53.0	56.0	15.2	200.1	4111.0
	6E	1295.0	152.3	41.5	34.0	15.2	200.1	2933.2
	7E	1512.0	102.4	30.0	12.0	15.2	200.1	1755.4
	8E	1729.0	52.5	18.5	0.0	15.2	200.1	577.6
	9E	1946.0	2.6	7.0	-1.5	15.2	200.1	-400.2
	10E	2163.0	-27.3	-15.0	-28.0	15.2	200.1	-822.4
300 x 100	1E	210	424.4	48.0	82.2	15.2	200.1	822.2
	2E	427.0	424.4	48.0	82.2	15.2	200.1	1644.4
	3E	644.0	376.4	76.0	110.0	15.2	200.1	2466.6
	4E	861.0	276.1	64.5	78.0	15.2	200.1	3288.8
	5E	1078.0	202.2	53.0	56.0	15.2	200.1	4111.0
	6E	1295.0	152.3	41.5	34.0	15.2	200.1	2933.2
	7E	1512.0	102.4	30.0	12.0	15.2	200.1	1755.4
	8E	1729.0	52.5	18.5	0.0	15.2	200.1	577.6
	9E	1946.0	2.6	7.0	-1.5	15.2	200.1	-400.2
	10E	2163.0	-27.3	-15.0	-28.0	15.2	200.1	-822.4

UNIVERSAL COLUMNS
Parallel Flanges

DIMENSIONS AND PROPERTIES

Serial No.	Moment of inertia				Radius of Gyration			Elastic Modulus	2nd D ₁ E
	Axis-1 C ₁₁	Axis-2 C ₂₂	Axis-3 C ₃₃	Axis-4 C ₄₄	Axis-1 r ₁₋₁	Axis-2 r ₂₋₂	Axis-3 r ₃₋₃		
300 x 400	270140	242070	88211	16.8	11.0	1502	4032	0.2	
	227023	200212	82845	18.0	10.8	8084	3981	0.0	
	183115	161031	87305	17.8	10.7	6358	3285	1.0	
	146715	120188	85410	17.1	10.5	5024	2723	0.0	
	132474	107807	88930	18.0	10.4	6077	2705	0.5	
	99611	87849	88714	18.5	10.3	5040	1940	0.8	
	79110	67424	87009	18.2	10.2	4183	1870	1.2	
	300 x 300	17287	15128	68097	16.8	10.0	3070	2507	0.0
		68207	51806	23632	18.0	9.17	3560	1480	10.8
		61750	40758	20670	15.0	9.32	2794	1100	15.8
48220		42250	17470	15.8	9.46	2081	843.0	13.5	
40246		28092	14556	15.0	9.20	1394	700.4	20.2	
300 x 200		18177	72827	24645	14.8	8.20	4274	1825	0.3
		64177	58028	20239	14.5	8.14	7641	1272	8.4
		50882	48938	18230	14.2	8.02	2911	1034	10.8
		38720	35766	12024	13.8	7.89	2208	808.3	12.1
		32828	30314	10872	13.7	7.62	2089	691.6	14.4
	27561	25472	9008	12.8	7.26	1755	587.0	16.0	
	22202	20486	7288	13.4	7.80	1442	478.9	20.0	
	200 x 200	20914	27171	9788	11.8	6.28	2070	740.8	3.1
		22416	20510	7444	17.8	6.46	1892	570.4	11.0
		17810	15880	8907	11.3	6.57	1012	458.8	13.0
14307		12578	4549	11.2	6.52	1098	378.9	15.1	
11260		10287	3878	11.1	6.48	8045	208.0	17.9	
150 x 150		9482	4374	3118	9.27	5.32	8515	288.7	10.8
		7647	8758	2528	8.18	5.28	7084	248.0	13.6
		8086	5303	2041	8.08	5.18	5831	198.0	14.8
		5203	4453	1770	8.50	5.19	6104	179.8	14.5
		4064	4025	1338	8.81	5.11	4682	157.8	16.5
	100 x 100	2218	1822	703	6.94	2.87	2742	81.78	14.1
		1742	1518	558	8.78	2.82	2212	73.08	18.9
		1262	1104	403	9.51	2.88	1687	62.98	21.4

Note: One side is deduced from next flange number. 200mm width (total) is used for calculation from each flange from www.easyvet.com and use Social media to calculate the 100 Moment of Inertia from 1-4.

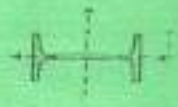




UNIVERSAL BEAMS

DIMENSIONS AND PROPERTIES

Serial Size	Mass per meter	Depth of Section D	Width of Section B	Thickness			Root Radius r	Depth of Flange e	Area of Section cm ²
				Web t	Flange T	Flange t			
610 x 410	388	420.5	418.5	21.5	26.0	24.1	101.2	430.8	
614 x 308	343	311.4	418.5	19.4	22.0	24.1	79.2	400.3	
610 x 228	140	230.1	230.1	13.1	22.1	12.7	64.1	194.2	
610 x 208	128	207.2	207.2	11.9	20.0	12.7	57.1	174.4	
610 x 178	81	178.4	178.4	10.1	18.0	12.7	54.7	154.4	
528 x 220	110	258.8	258.8	14.8	23.7	12.7	79.2	210.2	
528 x 200	102	235.5	235.5	13.2	21.0	12.7	71.8	194.2	
528 x 185	88	215.4	215.4	12.8	19.5	12.7	64.1	180.2	
487 x 171	61	185.4	185.4	9.2	17.8	12.7	47.8	138.2	



UNIVERSAL BEAMS

DIMENSIONS AND PROPERTIES

Serial Size	Moments of Inertia			Radius of Gyration			Elastic Modulus			Stain D _y
	Axis	Axis	Axis	Axis	Axis	Axis	Axis	Axis	Axis	
614 x 410	717330	829177	47481	38.1	52.7	15000	2021	26.2		
614 x 308	503781	489802	30221	27.0	42.1	10078	1732	18.0		
610 x 228	207152	192502	14972	14.7	34.2	7371	574.4	10.2		
610 x 208	149202	140202	10571	10.5	30.8	6523	482.8	8.8		
610 x 178	85370	80076	1203	8.5	25.7	5078	381	7.1		
528 x 220	101889	154106	822	28.0	49.0	12000	194.2	27.9		
528 x 200	84408	137928	628	23.8	42.8	10000	174.4	21.2		
528 x 185	68132	120150	558	21.2	38.2	8000	154.4	18.0		
487 x 171	40049	82715	328	18.0	32.8	6000	118.2	13.1		

TABLE 2

TABLE 3:
ALLOWABLE STRESS p_c ON GROSS SECTION
FOR AXIAL COMPRESSION

λ_r	p_c (N/mm ²) for grade 43 steel									
	0	1	2	3	4	5	6	7	8	9
0	155	155	154	154	153	153	153	152	152	151
10	151	151	150	150	149	149	148	148	147	147
20	147	146	146	146	145	145	144	144	143	143
30	143	142	142	142	141	141	140	140	139	139
40	139	138	138	137	137	136	136	135	134	134
50	135	134	134	133	133	132	132	131	130	130
60	130	129	129	128	128	127	127	126	125	125
70	125	124	124	123	123	122	122	121	120	120
80	120	119	119	118	118	117	117	116	115	115
90	114	113	113	112	112	111	111	110	109	109
100	109	108	108	107	107	106	106	105	104	104
110	103	102	102	101	101	100	100	99	98	98
120	97	96	96	95	95	94	94	93	92	92
130	91	90	90	89	89	88	88	87	86	86
140	85	84	84	83	83	82	82	81	80	80
150	79	78	78	77	77	76	76	75	74	74
160	73	72	72	71	71	70	70	69	68	68
170	67	66	66	65	65	64	64	63	62	62
180	61	60	60	59	59	58	58	57	56	56
190	55	54	54	53	53	52	52	51	50	50
200	49	48	48	47	47	46	46	45	44	44
210	43	42	42	41	41	40	40	39	38	38
220	37	36	36	35	35	34	34	33	32	32
230	31	30	30	29	29	28	28	27	26	26
240	25	24	24	23	23	22	22	21	20	20
250	19	18	18	17	17	16	16	15	14	14
260	13	12	12	11	11	10	10	9	8	8
270	7	6	6	5	5	4	4	3	2	2
280	1	0	0	0	0	0	0	0	0	0
290	0	0	0	0	0	0	0	0	0	0
300	0	0	0	0	0	0	0	0	0	0
350	0	0	0	0	0	0	0	0	0	0
400	0	0	0	0	0	0	0	0	0	0
450	0	0	0	0	0	0	0	0	0	0
500	0	0	0	0	0	0	0	0	0	0

Intermediate values may be obtained by linear interpolation.

NOTE: For material over 40 mm thick, other than rolled I-beams or channels, and for Universal columns of thickness exceeding 40 mm, the limiting stress is 140 N/mm².

TABLE 4

Modification factor K_{12} for compression members		Value of K_{12}																				
		Values of slenderness ratio λ ($=L_e/r$)																				
		< 5	5	10	20	30	40	50	60	70	80	90	100	120	140	160	180	200	220	240	250	
$F_{t,c,1}$	Equivalent L_e/r (for rectangular sections)																					
		< 14	14	29	58	87	115	145	175	202	231	260	289	347	405	452	520	579	636	694	723	
400	1.000	0.975	0.951	0.898	0.827	0.735	0.621	0.506	0.408	0.330	0.271	0.225	0.182	0.121	0.094	0.075	0.061	0.051	0.043	0.040		
500	1.000	0.975	0.951	0.899	0.837	0.759	0.664	0.562	0.468	0.385	0.320	0.269	0.199	0.148	0.115	0.092	0.076	0.063	0.053	0.048		
600	1.000	0.975	0.951	0.901	0.843	0.774	0.692	0.601	0.511	0.430	0.367	0.307	0.226	0.172	0.135	0.109	0.089	0.074	0.063	0.058		
700	1.000	0.975	0.951	0.902	0.848	0.784	0.711	0.629	0.545	0.467	0.399	0.341	0.264	0.195	0.154	0.124	0.102	0.085	0.072	0.067		
800	1.000	0.975	0.952	0.903	0.851	0.792	0.724	0.649	0.572	0.497	0.430	0.371	0.280	0.217	0.172	0.139	0.115	0.096	0.082	0.076		
900	1.000	0.976	0.952	0.904	0.853	0.787	0.734	0.665	0.590	0.522	0.456	0.397	0.304	0.237	0.188	0.153	0.127	0.106	0.091	0.084		
1000	1.000	0.976	0.952	0.904	0.855	0.801	0.742	0.677	0.609	0.542	0.478	0.420	0.325	0.255	0.204	0.167	0.138	0.116	0.099	0.092		
1100	1.000	0.976	0.952	0.906	0.856	0.804	0.748	0.687	0.623	0.559	0.497	0.440	0.344	0.272	0.219	0.179	0.149	0.126	0.107	0.100		
1200	1.000	0.976	0.952	0.905	0.857	0.807	0.753	0.695	0.634	0.573	0.513	0.457	0.362	0.288	0.233	0.182	0.150	0.135	0.116	0.107		
1300	1.000	0.976	0.952	0.905	0.858	0.809	0.757	0.701	0.643	0.584	0.527	0.472	0.378	0.303	0.247	0.203	0.170	0.144	0.123	0.115		
1400	1.000	0.976	0.952	0.906	0.859	0.811	0.760	0.707	0.651	0.595	0.539	0.486	0.392	0.317	0.259	0.214	0.180	0.153	0.131	0.122		
1500	1.000	0.976	0.952	0.906	0.860	0.813	0.763	0.712	0.658	0.603	0.550	0.498	0.405	0.330	0.271	0.226	0.189	0.161	0.138	0.129		
1600	1.000	0.976	0.952	0.906	0.861	0.814	0.768	0.716	0.664	0.611	0.559	0.508	0.417	0.342	0.282	0.235	0.198	0.169	0.145	0.135		
1700	1.000	0.976	0.952	0.906	0.861	0.815	0.768	0.719	0.669	0.618	0.567	0.518	0.428	0.353	0.292	0.245	0.207	0.177	0.152	0.142		
1800	1.000	0.976	0.952	0.906	0.862	0.816	0.770	0.722	0.673	0.624	0.574	0.526	0.438	0.363	0.302	0.254	0.215	0.184	0.159	0.149		
1900	1.000	0.976	0.952	0.907	0.862	0.817	0.772	0.725	0.677	0.629	0.581	0.534	0.447	0.373	0.312	0.262	0.223	0.191	0.165	0.154		
2000	1.000	0.976	0.952	0.907	0.863	0.818	0.773	0.728	0.681	0.634	0.587	0.541	0.455	0.382	0.320	0.271	0.230	0.198	0.172	0.160		

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